Verification of a Finite Element Model for Pyrolyzing Ablative Materials

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Outline

- Objective
- General Pyrolyzing Ablator Problem
- Solution Examples Using Finite Element Model
  - Thermogravimetric Analysis (TGA)
  - One-Dimensional Steady-State Profile
  - One-Dimensional Transient
  - Two-Dimensional Transient
- Summary and Conclusions

Objective

- NASA primarily relies on custom written codes to analyze ablation and design TPS systems
- The basic modeling methodology was developed 50 years ago
- Through the years, CFD, thermal, and structural mechanics calculations have migrated from custom, user-written programs to commercial software packages
- Objective is to determine that a commercial finite element code can accurately and efficiently solve pyrolyzing ablation problems

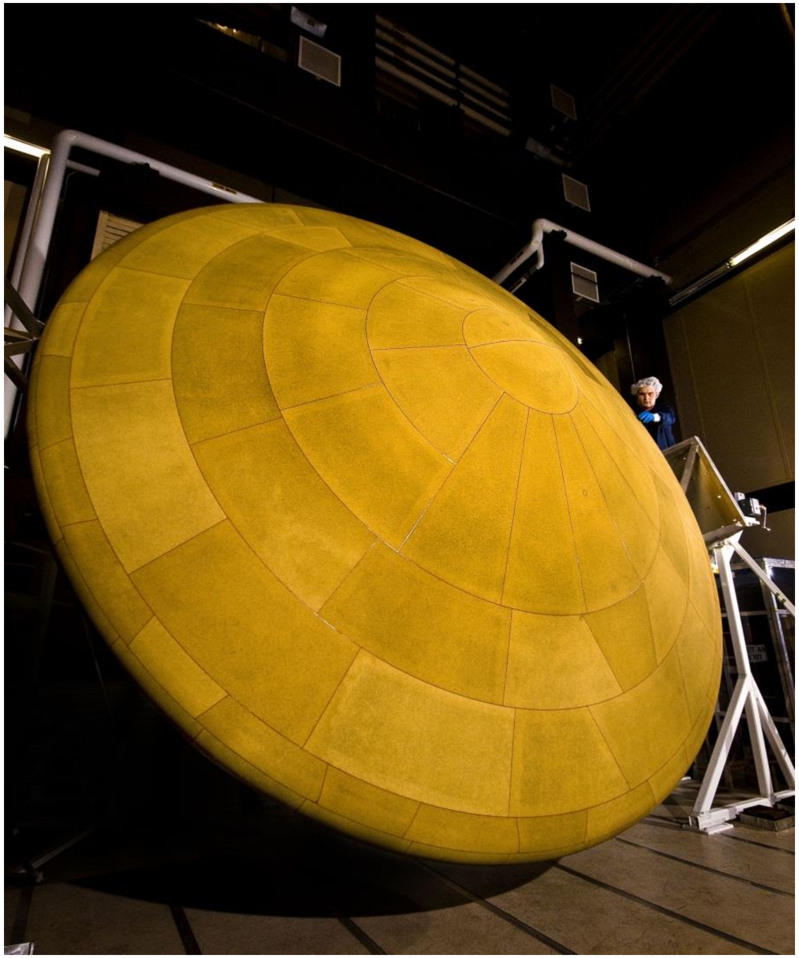
Advantages of Commercial Codes

- Usability (e.g. GUI)
- Built–in pre- and post-processing
- Built-in grid generation
- Efficient solution algorithms
- Multi-dimensional capability (planar, cylindrical, 1-D, 2-D, & 3-D)
- Built in function capability (predefined, analytic, and tabular)
- Validated by a wide user base
- Reduced life cycle cost
- Regular upgrades and maintenance
- Modeling flexibility
- Better documentation

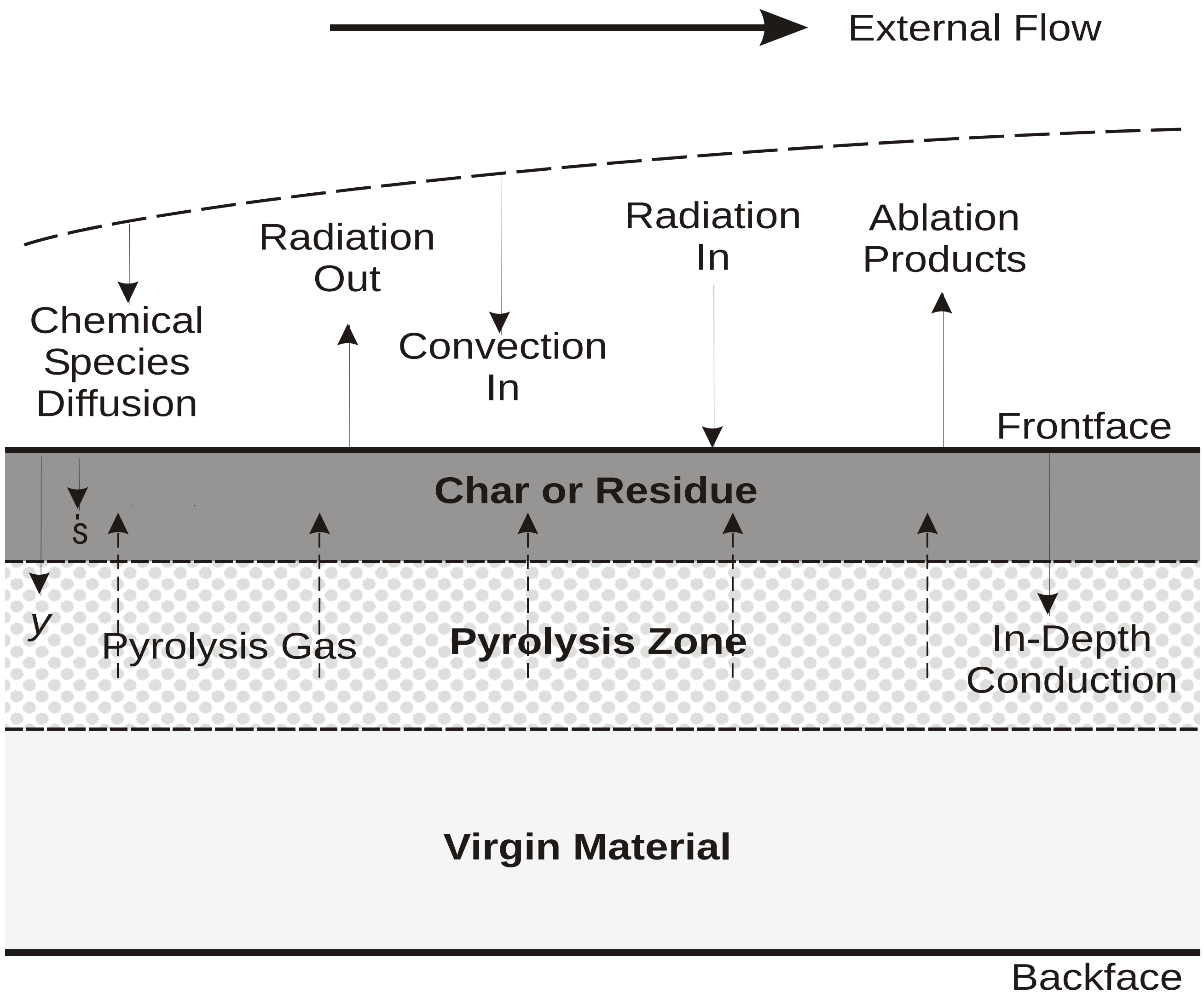
Finite-Element Program Choice

- COMSOL Multiphysics® chosen as simulation platform
- General-purpose software platform
  - Developed to handle wide variety of modeling physics
  - Allows arbitrarily inclusions of differential and algebraic modeling equations in domains, along boundaries, and at points
- Solvers based on advanced numerical methods
- Arbitrary Lagrangian-Eulerian (ALE) capability (moving boundary)
- Dynamic grid reallocation
- Flexible solution algorithms (fully coupled and sequential)
- Provides coupling between physical phenomena
- Incorporates automation and optimization capabilities
- Unified user interface (formulation, gridding, plotting, animation, & reporting)

Example Uses of Pyrolyzing Ablator



General Problem Illustration



Modeling Requirements for Pyrolyzing Ablators

- Non-linear heat conduction in solids
- Non-linear, thermal boundary conditions
- Moving boundaries
- Non-linear, time-dependent quasi-solid in-depth reactions
- Transport and thermal properties as a function of material state as well as temperature
- Inclusion of the thermal effects of gas flow within the solid material
- In-depth pore pressure due to pyrolysis gas transport (not always employed)

Decomposition Model

- Material consists of three constituents (although the number could be increased)

$$\rho = \Gamma(\rho_A + \rho_B) + (1 - \Gamma)\rho_C$$

- Components A and B decompose according to:

$$\left(\frac{\partial \rho_i}{\partial t}\right)_y = -A_i \exp\left(-\frac{E_i}{RT}\right)\rho_{o,i}\left(\frac{\rho_i - \rho_{r,i}}{\rho_{o,i}}\right)^{\psi_i}$$

- Material properties are a function not only of temperature, but also material state

Temperature History

- In-depth temperature time history can come from:
  - Thermogravimetric Analysis (TGA)

$$T = \beta t + T_0$$

  - Steady-State energy balance (1-D transformed coordinate)

$$\frac{\partial}{\partial y}\left(k\frac{\partial T}{\partial y}\right) + \left(\frac{\partial \dot{m}_g h_g}{\partial y}\right) + \dot{s}\left(\frac{\partial \rho h_s}{\partial y}\right) = 0$$

  - Transient energy balance (1-D transformed coordinate)

$$\rho C_p\left(\frac{\partial T}{\partial t}\right)_y = \frac{1}{A}\frac{\partial}{\partial y}\left(kA\frac{\partial T}{\partial y}\right)_t - \bar{h}(T)\left(\frac{\partial \rho}{\partial t}\right)_y + \dot{s}\rho C_p\left(\frac{\partial T}{\partial y}\right)_t + \frac{1}{A}\left(\frac{\partial \dot{m}_g h_g A}{\partial y}\right)_t$$

  - Transient Energy Balance (2-D fixed coordinate)

$$\rho C_p\left(\frac{\partial T}{\partial t}\right) = \frac{1}{A}\nabla(kA\nabla T) - \bar{h}(T)\left(\frac{\partial \rho}{\partial t}\right) + \frac{1}{A}\nabla\cdot\left(\dot{\boldsymbol{m}}_{\boldsymbol{g}} h_g A\right)$$

Material Selection

- For comparisons, utilize Theoretical Ablative Composite for Open Testing (TACOT) Material Properties
- Open, simulated pyrolyzing ablator that has been used a baseline test case for modeling ablation and comparing various predictive models
- Properties Required
  - Solid virgin and char specific heat, enthalpy, thermal conductivity, absorptivity and emissivity
  - Pyrolysis gas enthalpy
  - Surface thermochemistry mass loss and gas phase enthalpy

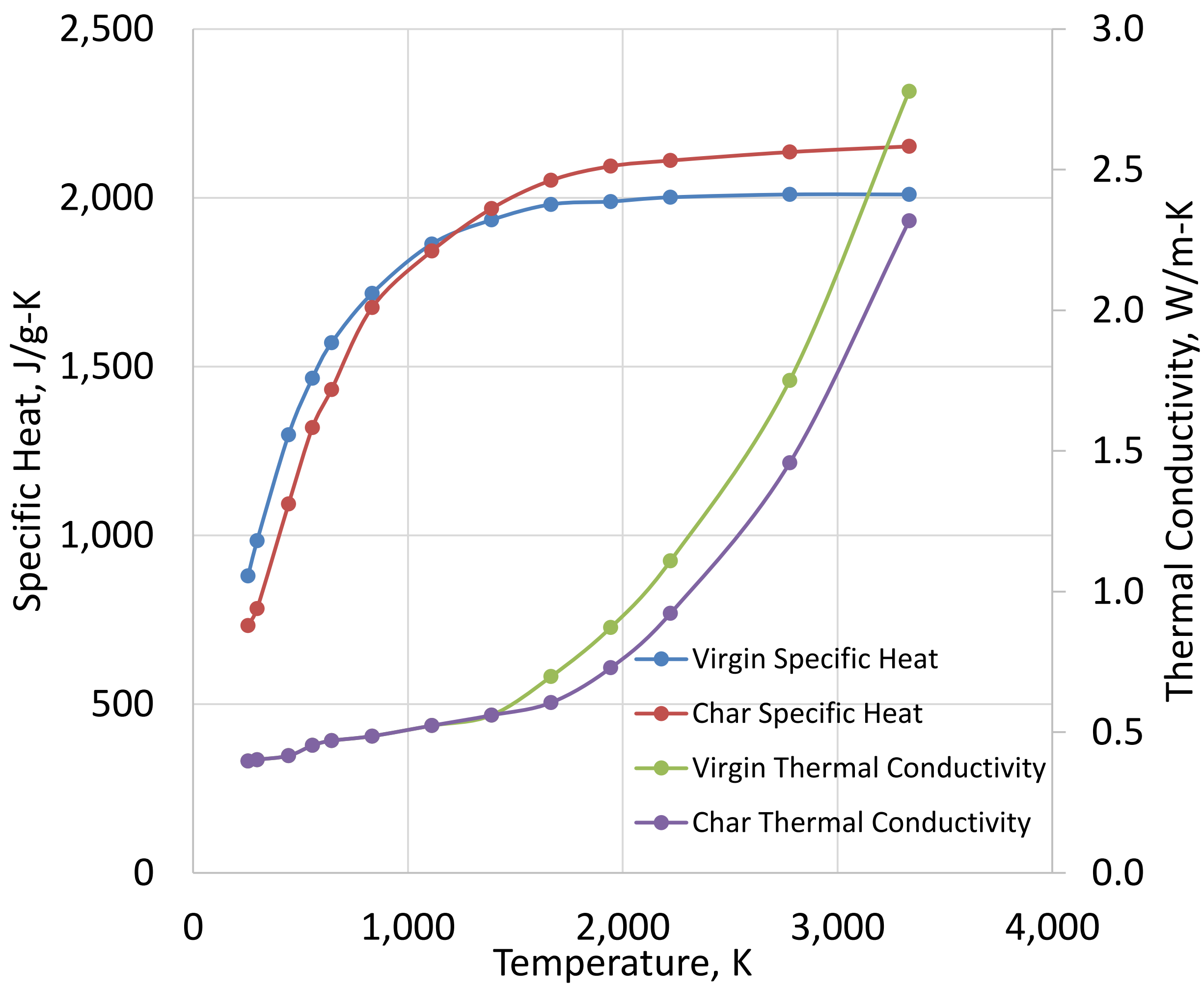
Thermophysical Properties

Thermophysical properties defined separately for virgin and char constituents. Composite properties determined by mixing rule based on mass.

$$k = xk_v + (1-x)k_c$$

$$C_p = xC_{p,v} + (1-x)C_{p,c}$$

$$x = \frac{\rho_v}{\rho_v - \rho_c}\left(1 - \frac{\rho_c}{\rho}\right)$$

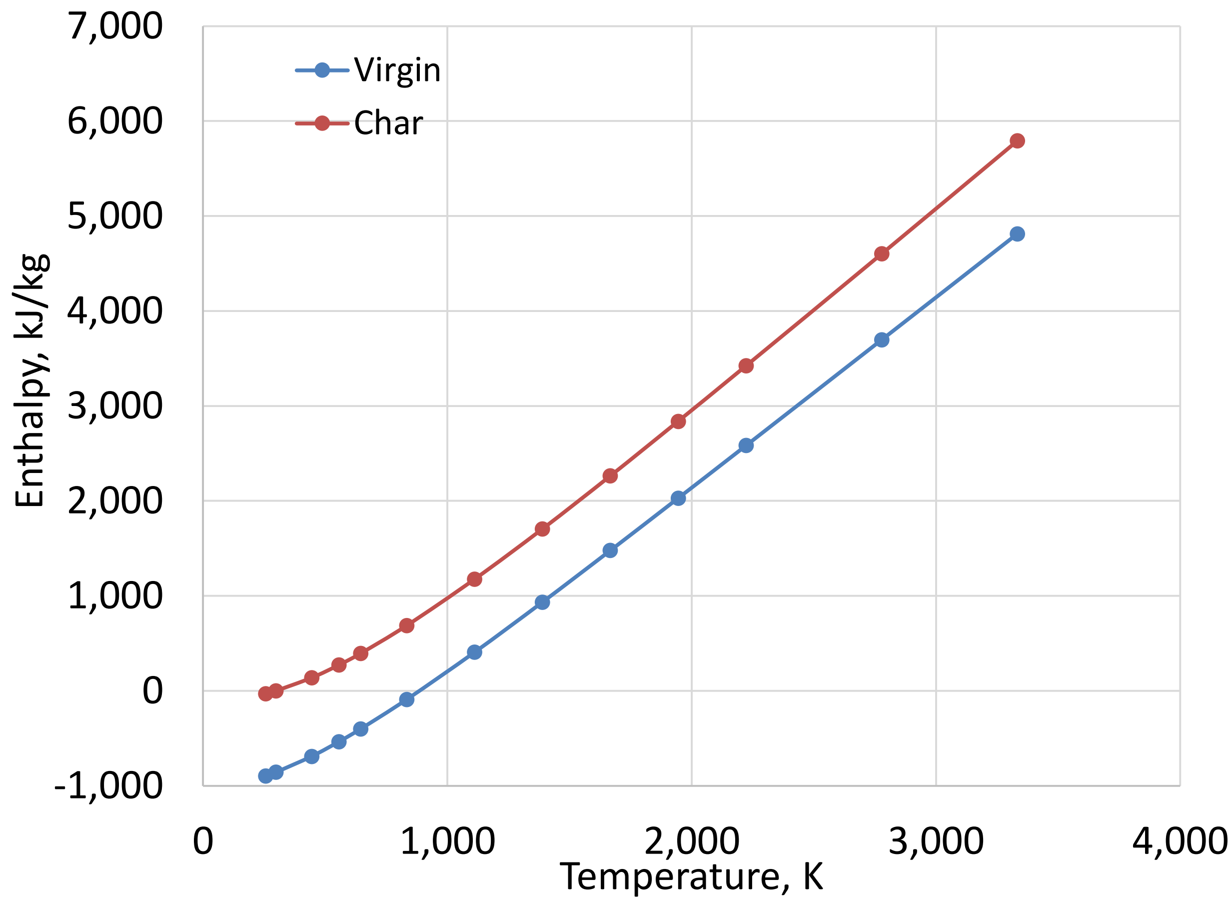


Material Enthalpy

Virgin and char enthalpies computed from integration of specific heats.

$$h = \int_{T_0}^{T} C_p dT + h_0$$

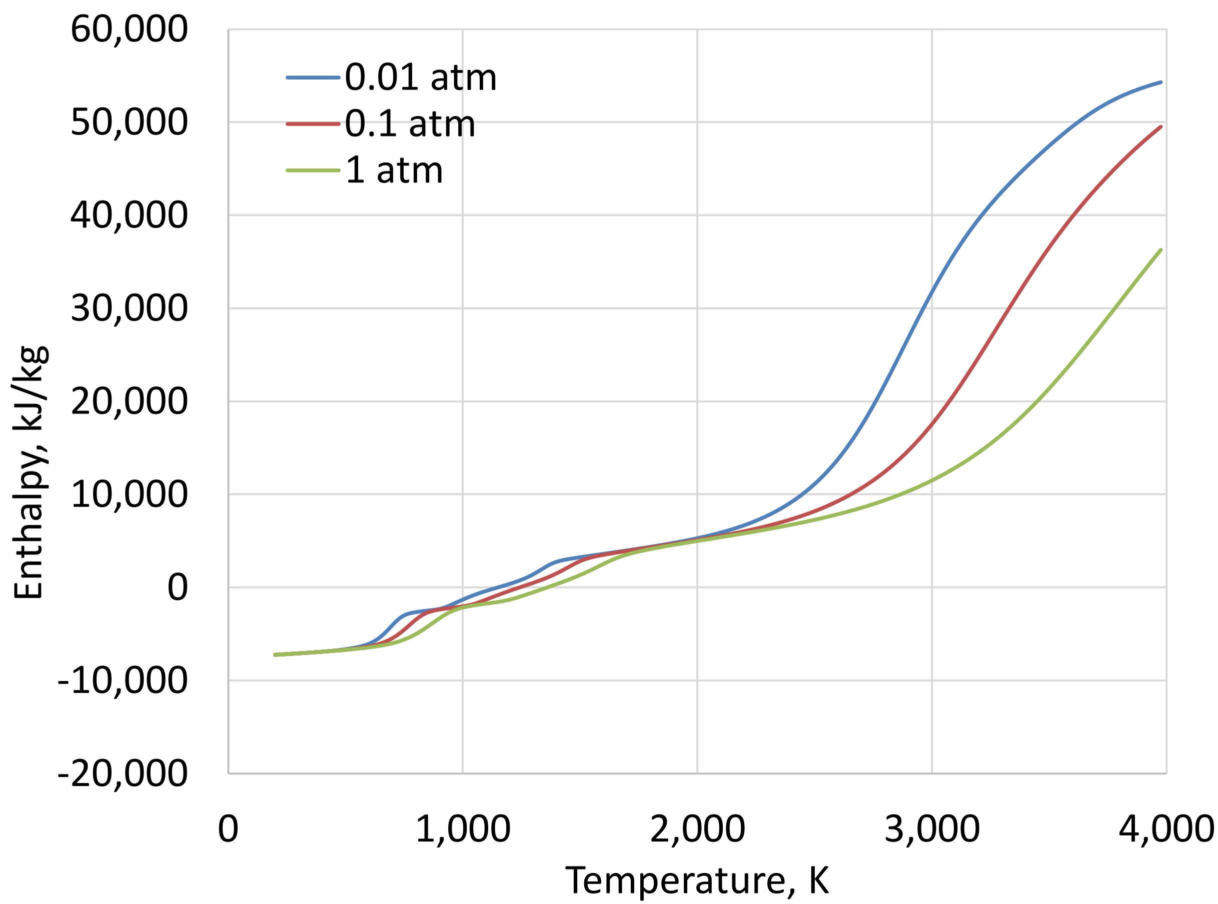
$$h = x h_v + (1 - x) h_c$$



Pyrolysis Gas Enthalpy

Pyrolysis gas enthalpy computed from equilibrium thermochemistry as a function of temperature and pressure.

$$h_{pg} = h_{pg}(p, T)$$

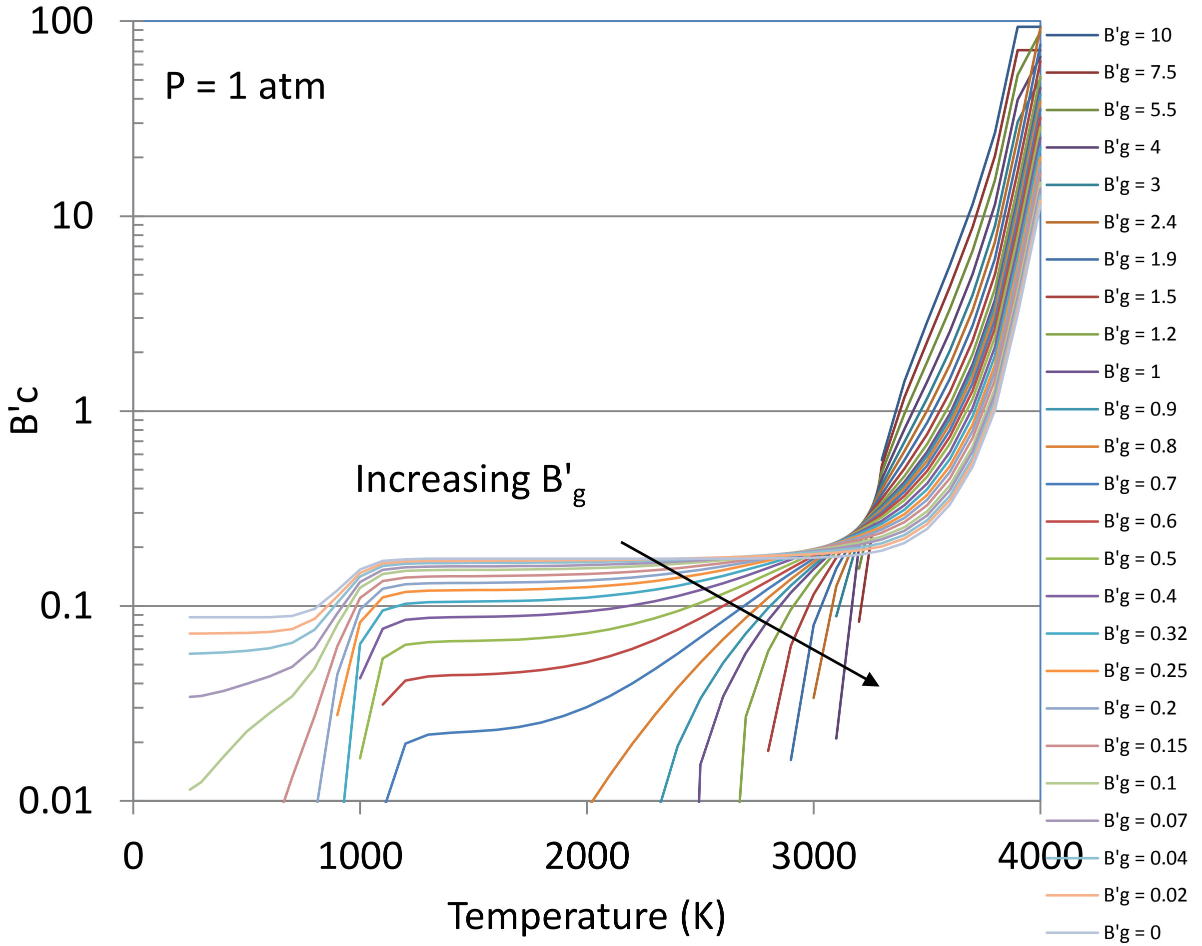


Surface Thermochemistry – Normalized Mass Loss

Surface thermochemistry conditions computed from equilibrium thermochemistry in terms of normalized mass fluxes.

$$B'_c = \dot{m}_c / \rho_e u_e C_M$$
$$B'_g = \dot{m}_g / \rho_e u_e C_M$$

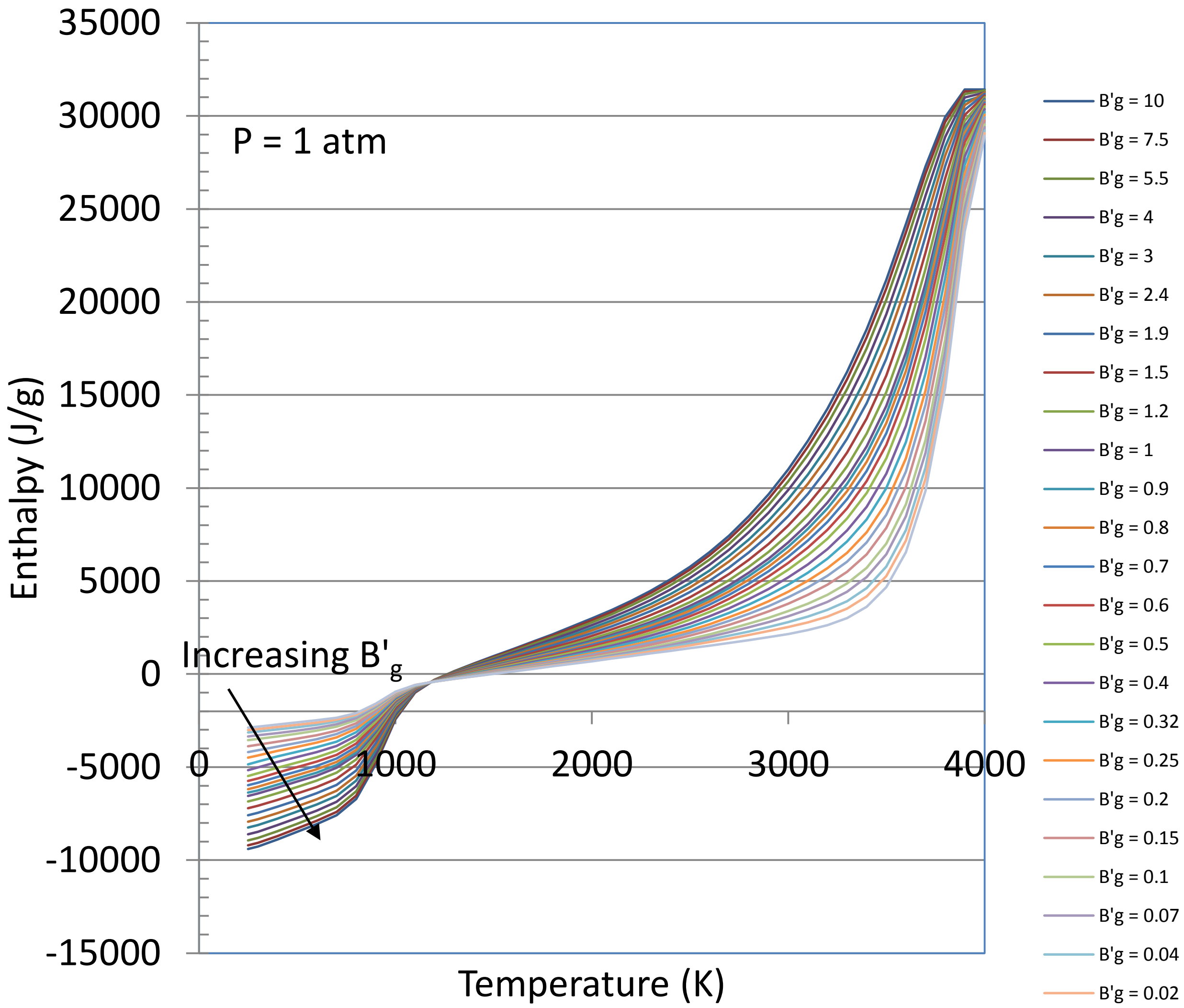
$$B'_c = B'_c(p, B'_g, T_s)$$



Surface Thermochemistry –Gas Phase Enthalpy

Enthalpy of gases at the wall computed similarly from equilibrium thermochemistry.

$$h_w = h_w(p, B'_g, T_s)$$



Example Problems

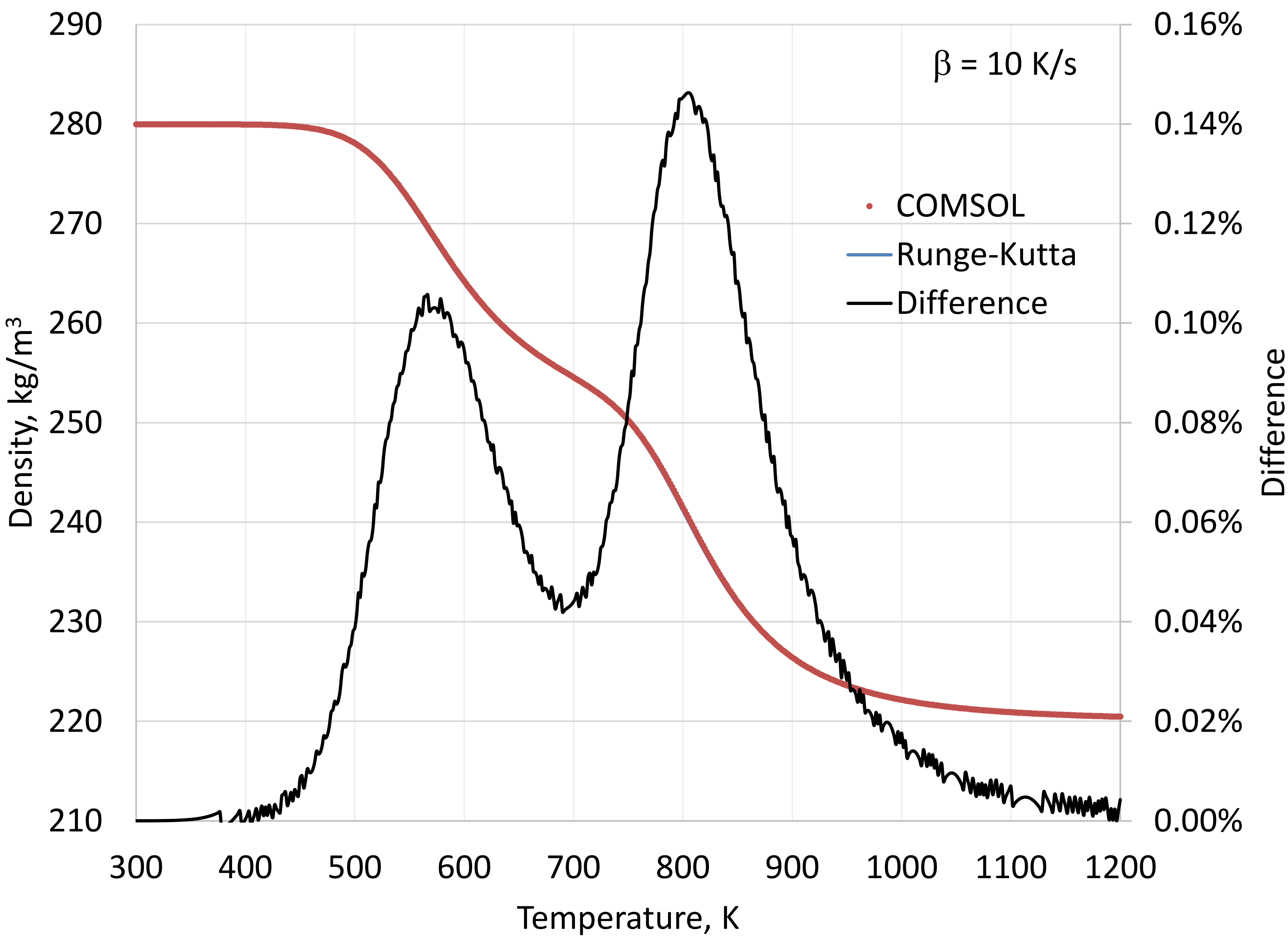
- Look at four examples
  - Thermogravimetric Analysis (TGA)
  - Steady-state one-dimensional thermal and density profile
  - One-dimensional transient temperature and recession history
  - Two-dimensional transient temperature and recession history

Thermogravimetric Analysis (TGA) Example

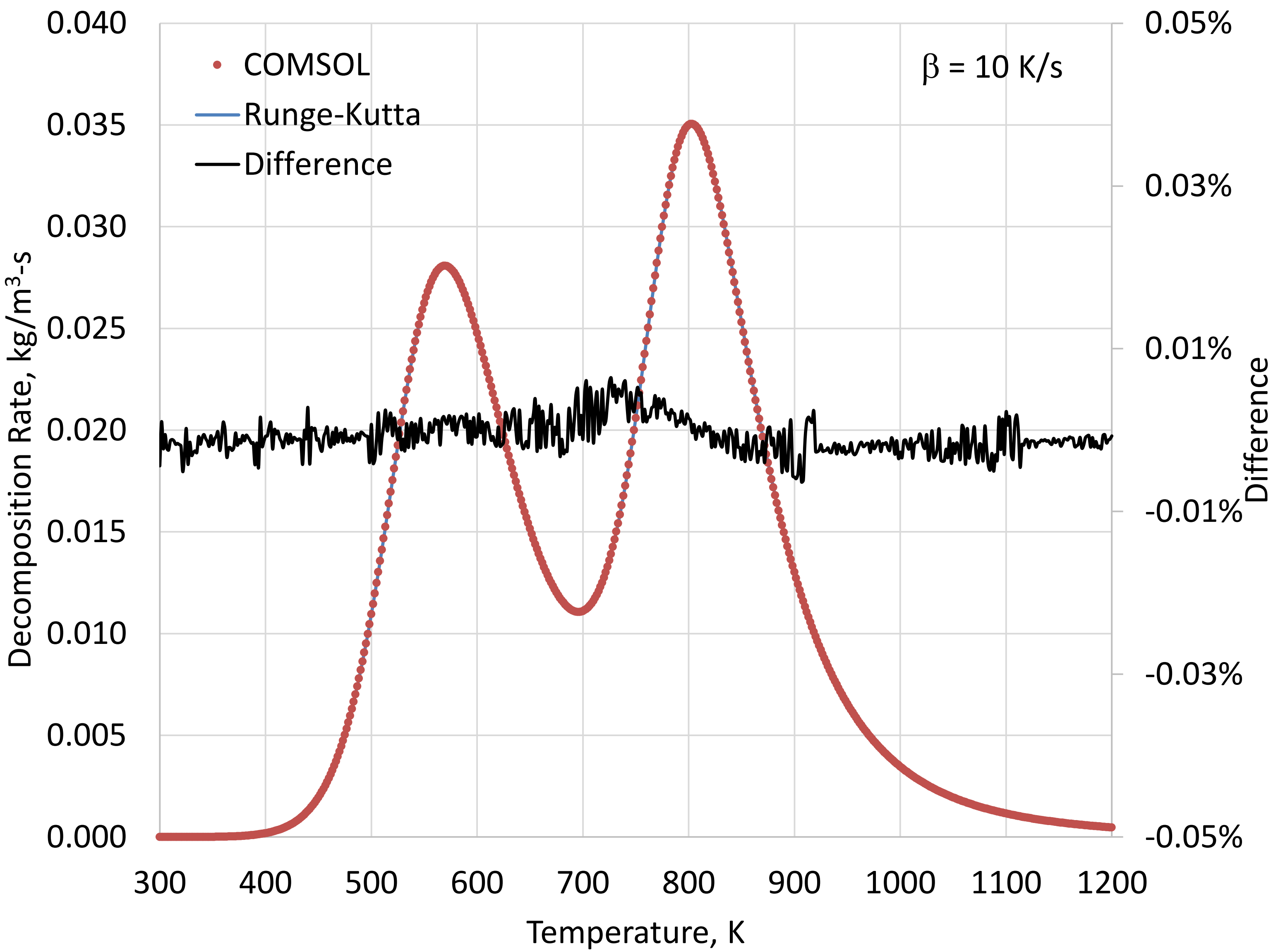
Thermogravimetric Analysis (TGA) Example

- Three component TACOT model
- Linear ramp increase in temperature at 10 K/s
- First-order time integration, not a spatial problem
- Results provide density and reaction rate for three components as a function of time
- COMSOL Multiphysics® results compared to independent fourth-order Runge-Kutta calculation

TGA Results - I



TGA Results - II

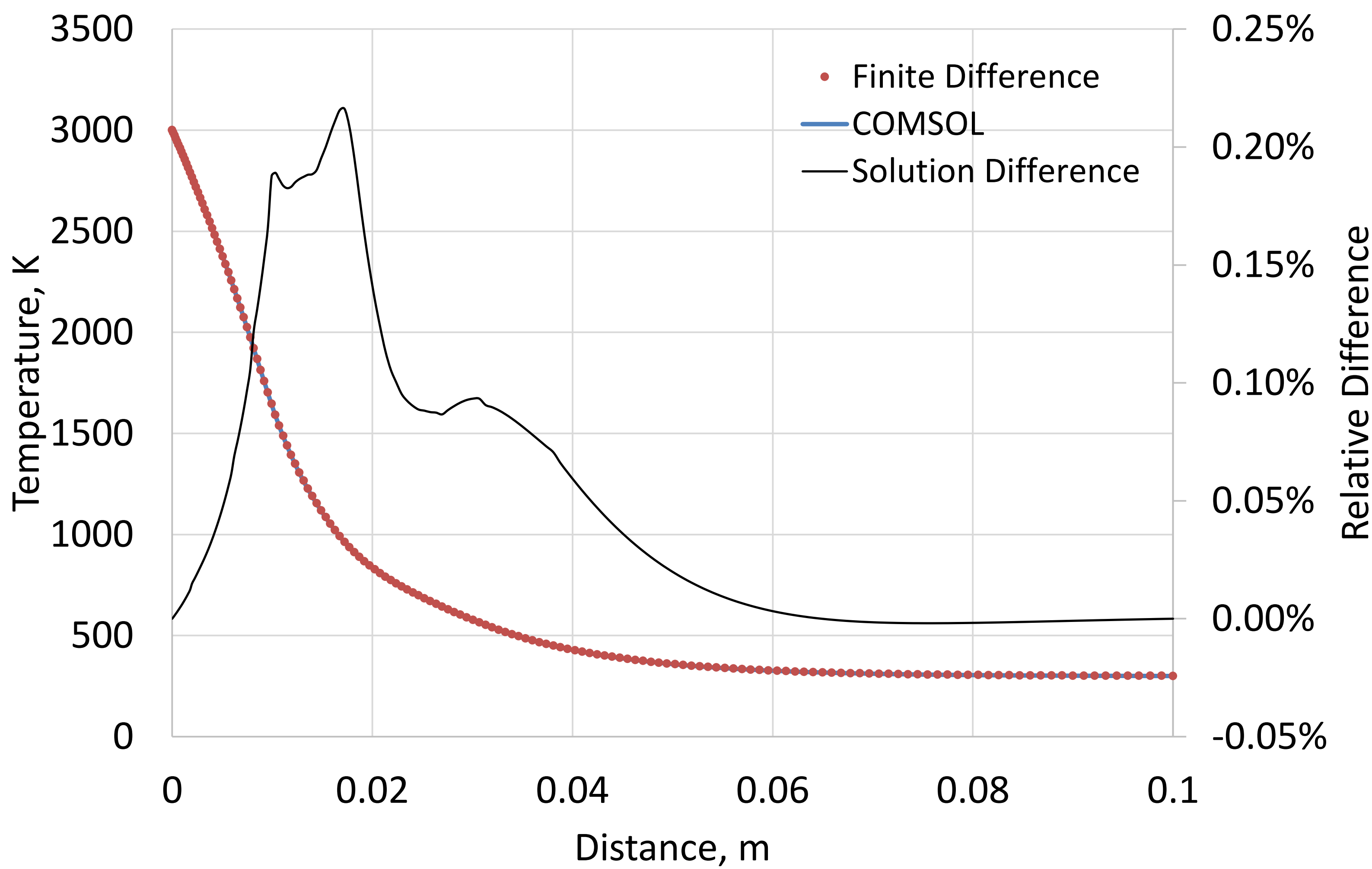


Steady-State Profile Example

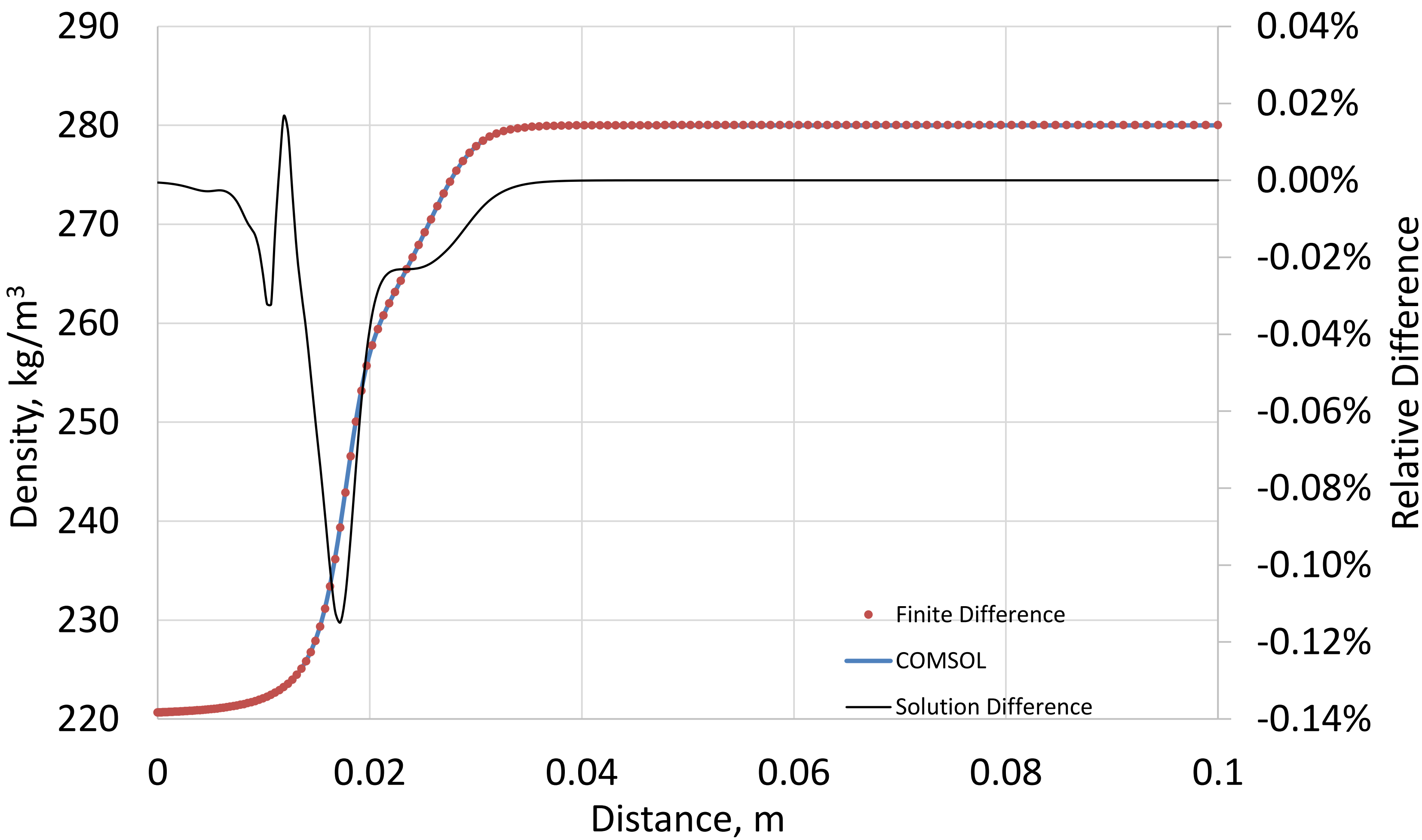
Steady-State Profile Example

- After long times in an infinite sample with a fixed surface temperature and recession, temperature and density profile will reach a steady state
- Problem solution becomes independent of time
- For this problem, specified surface temperature (3000 K) and recession rate (1×10^{-4} m/s) was used
- COMSOL Multiphysics® results compared to independent second order finite difference calculation and results from the Fully Implicit Ablation and Thermal Analysis Program (FIAT)

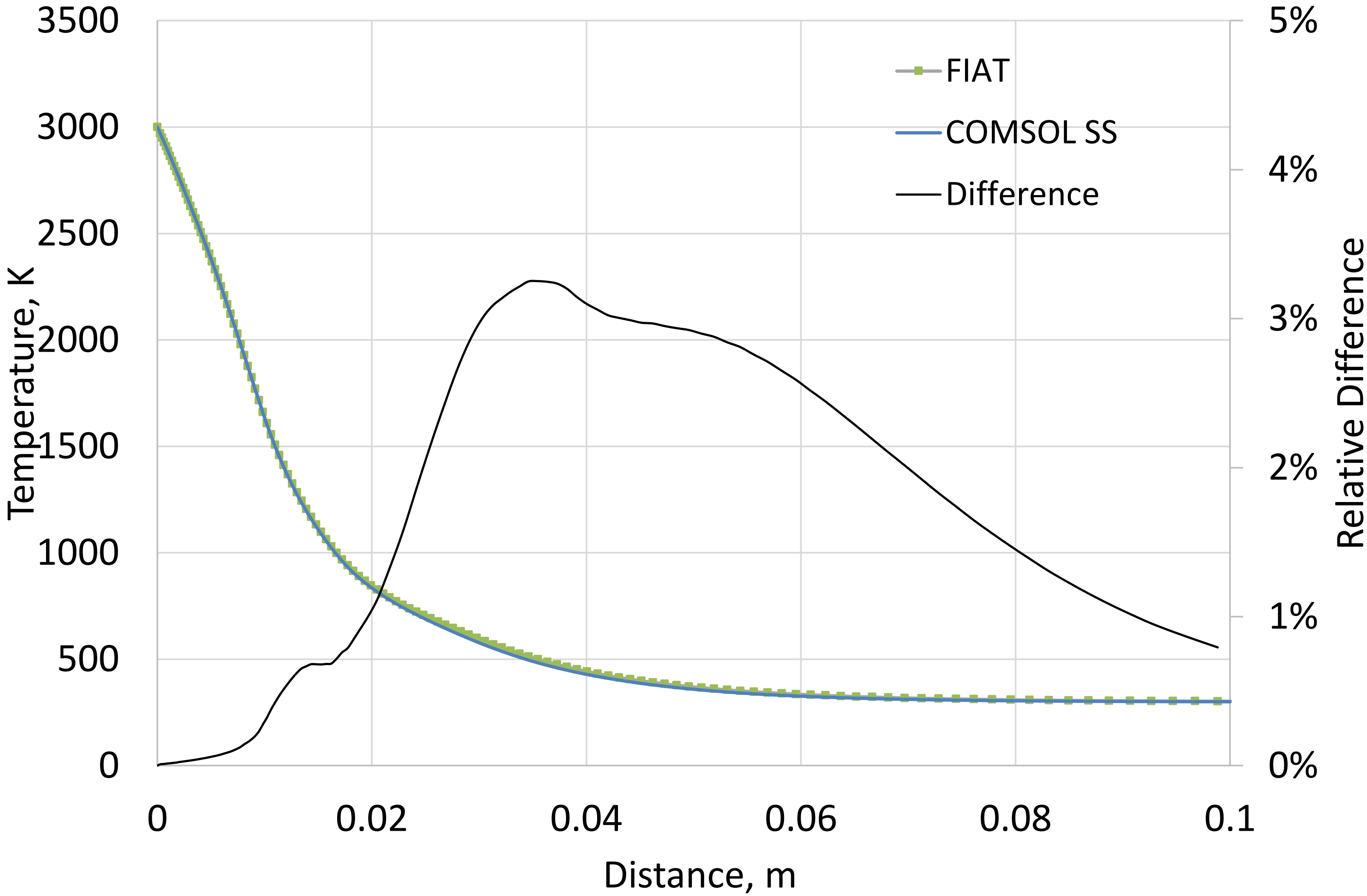
Finite Difference Temperature Profile Comparison



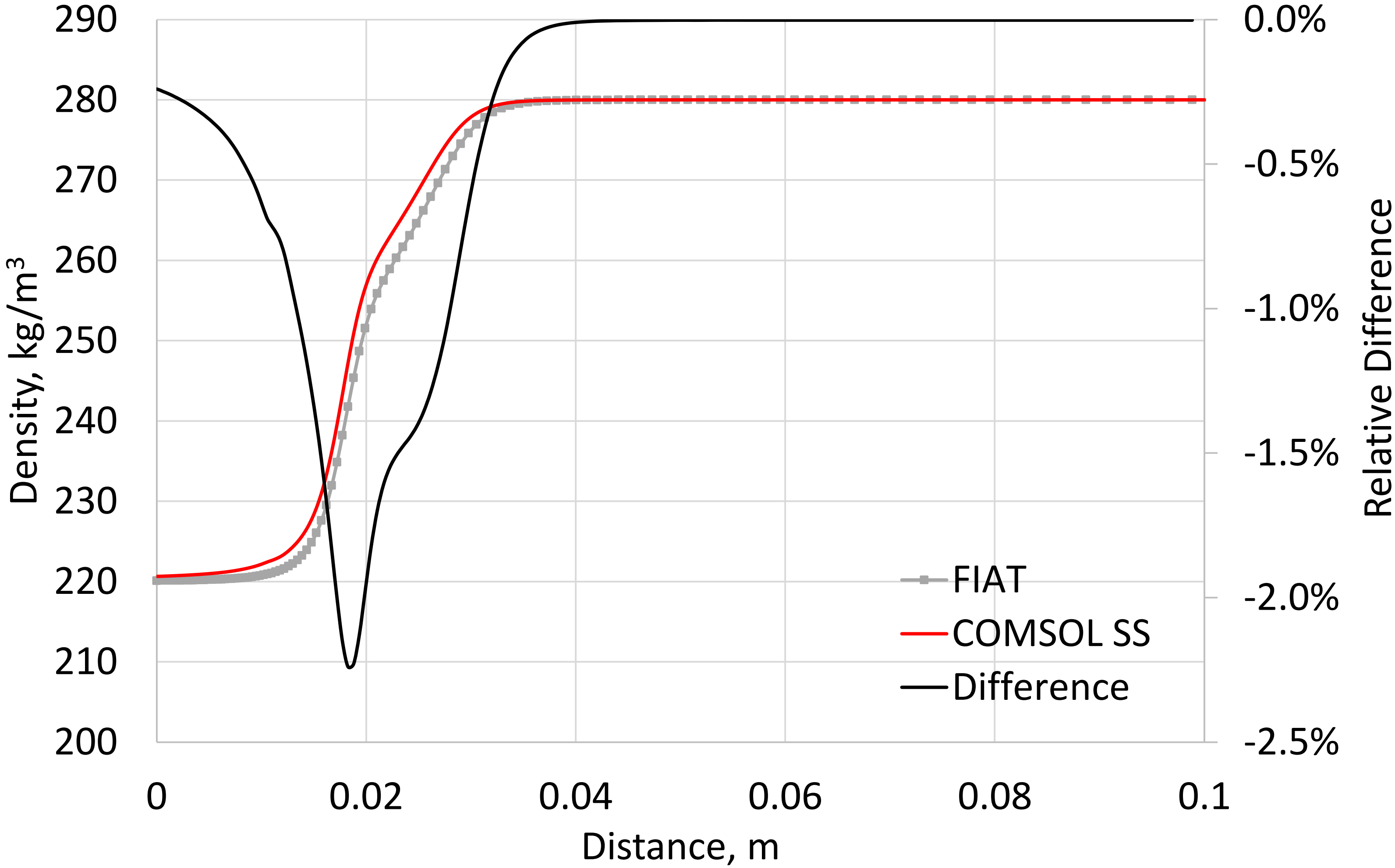
Finite Difference Density Profile Comparison



FIAT Temperature Profile Comparison



FIAT Density Profile Comparison

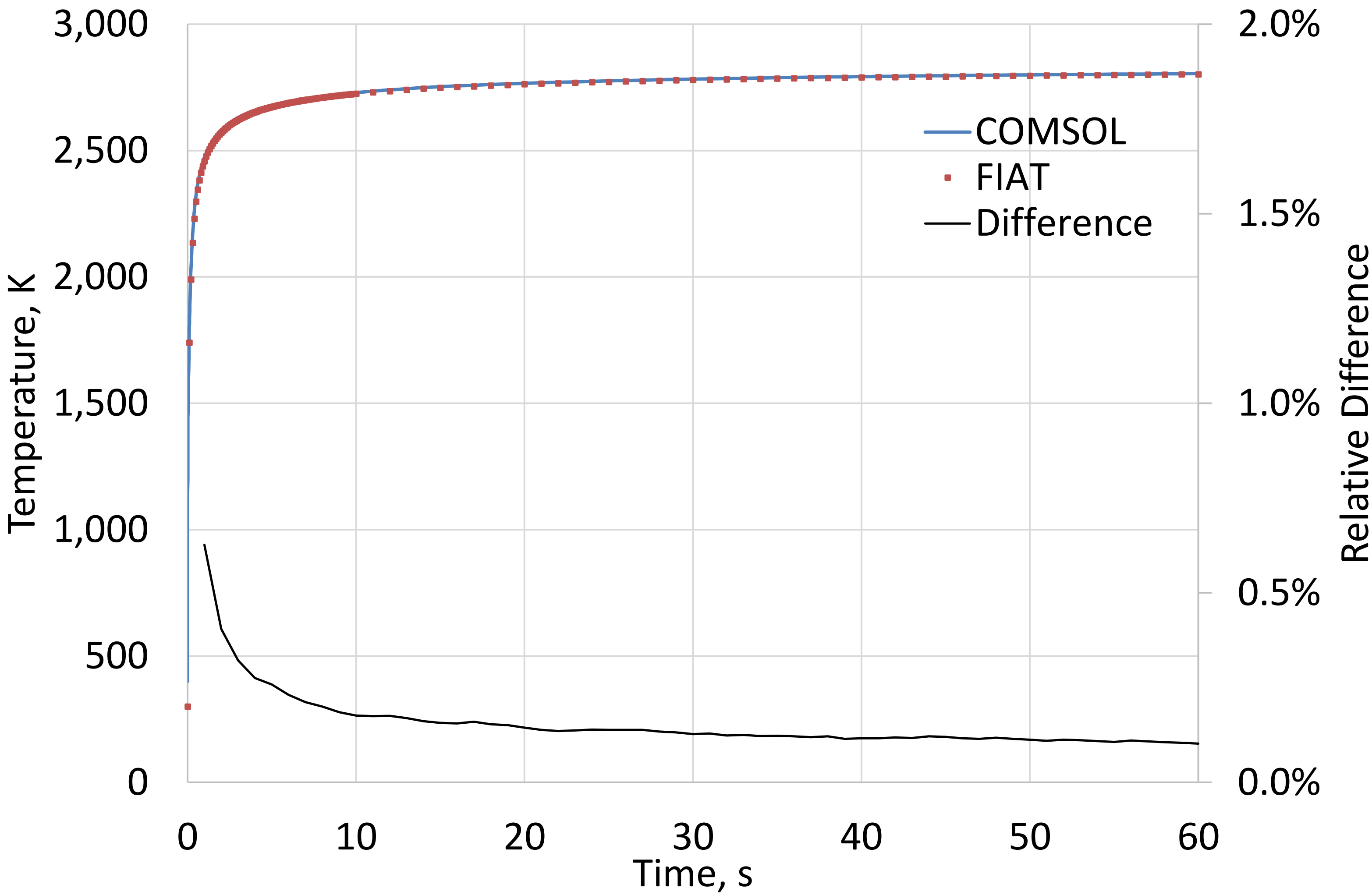


One-Dimensional Transient Example

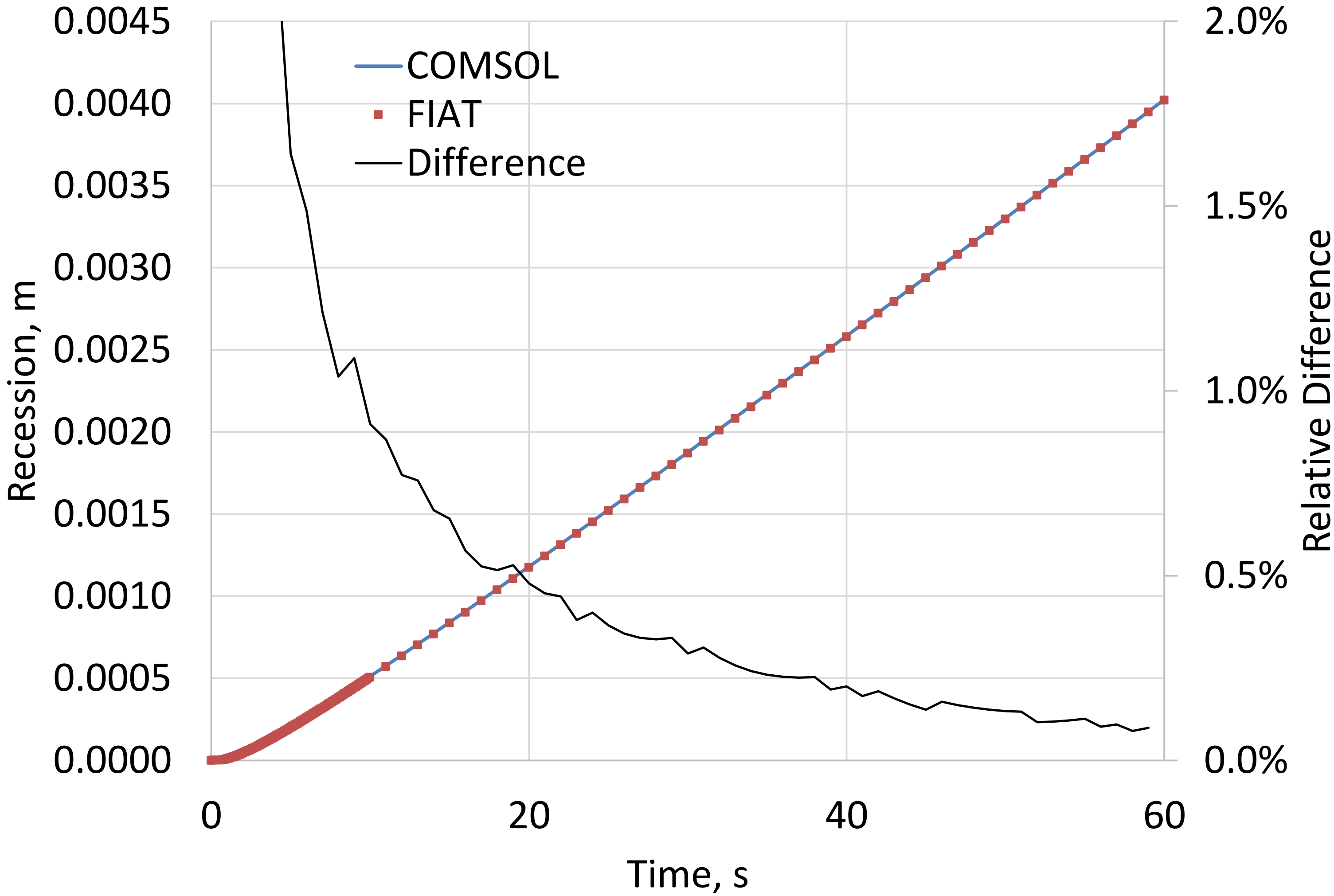
One-Dimensional Transient Example

- Problem is for a planar, finite width slab heated on one surface
- Full surface thermochemistry
- COMSOL Multiphysics® results compared to FIAT results

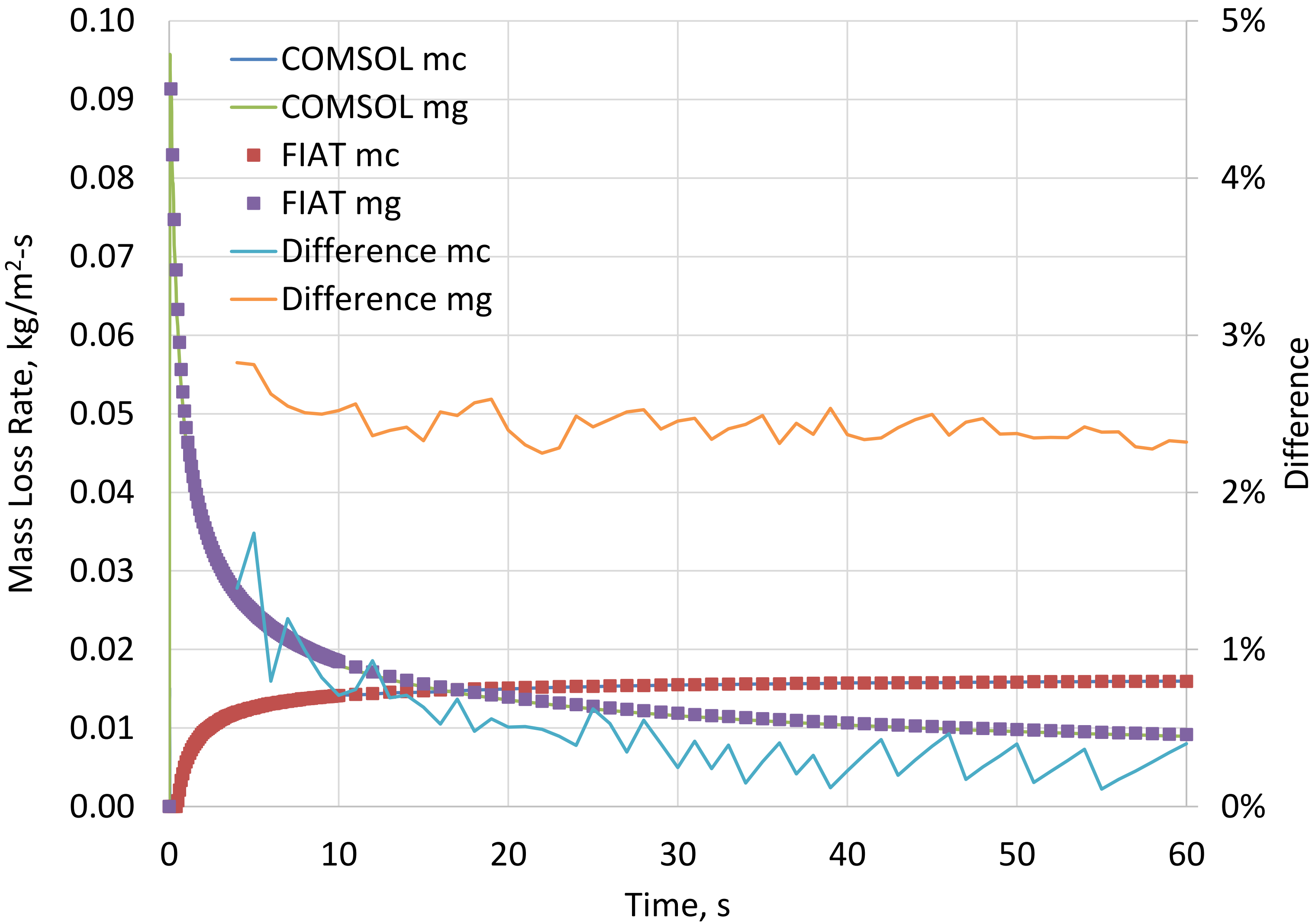
FIAT Surface Temperature Comparison



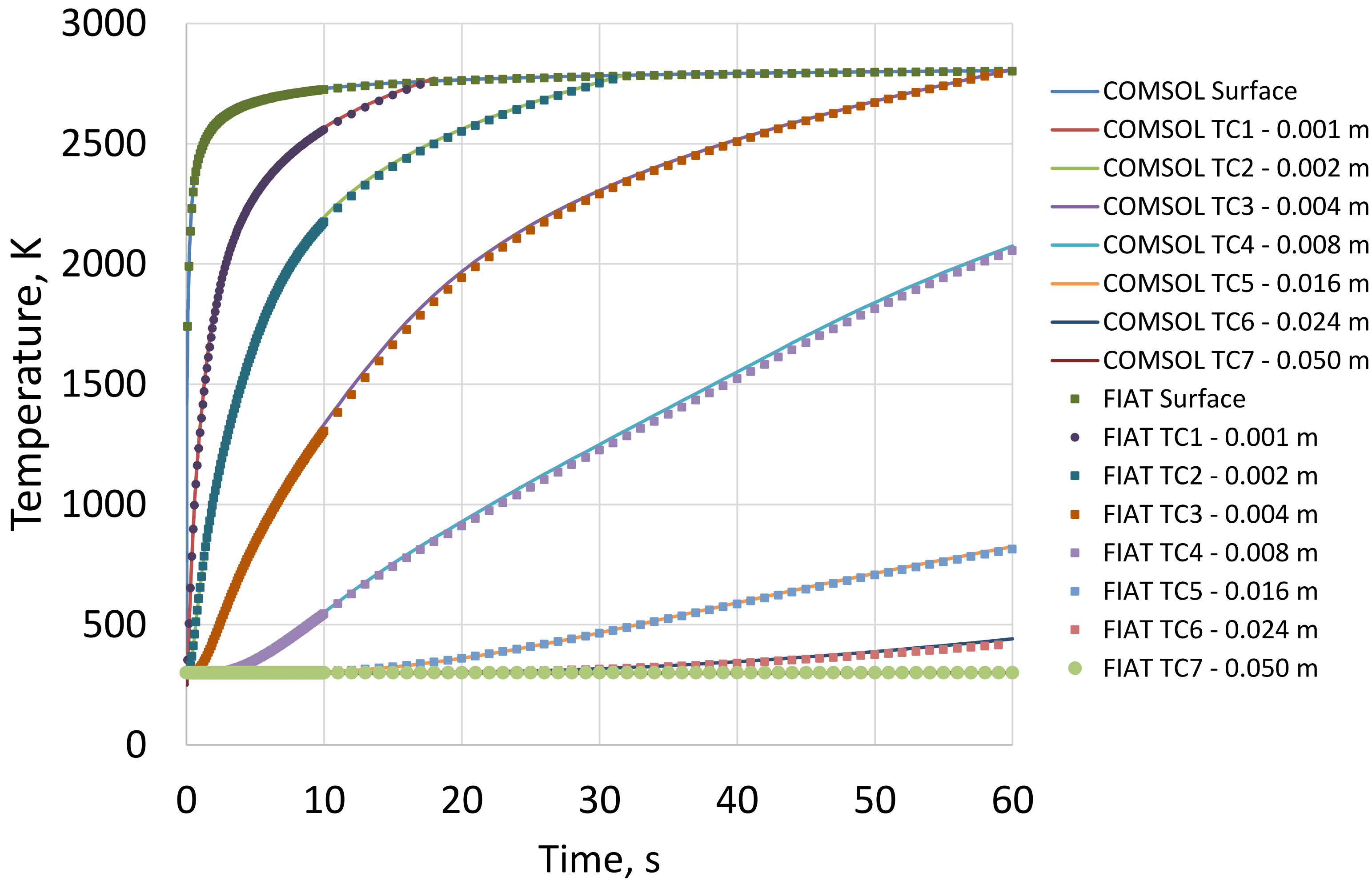
FIAT Recession Comparison



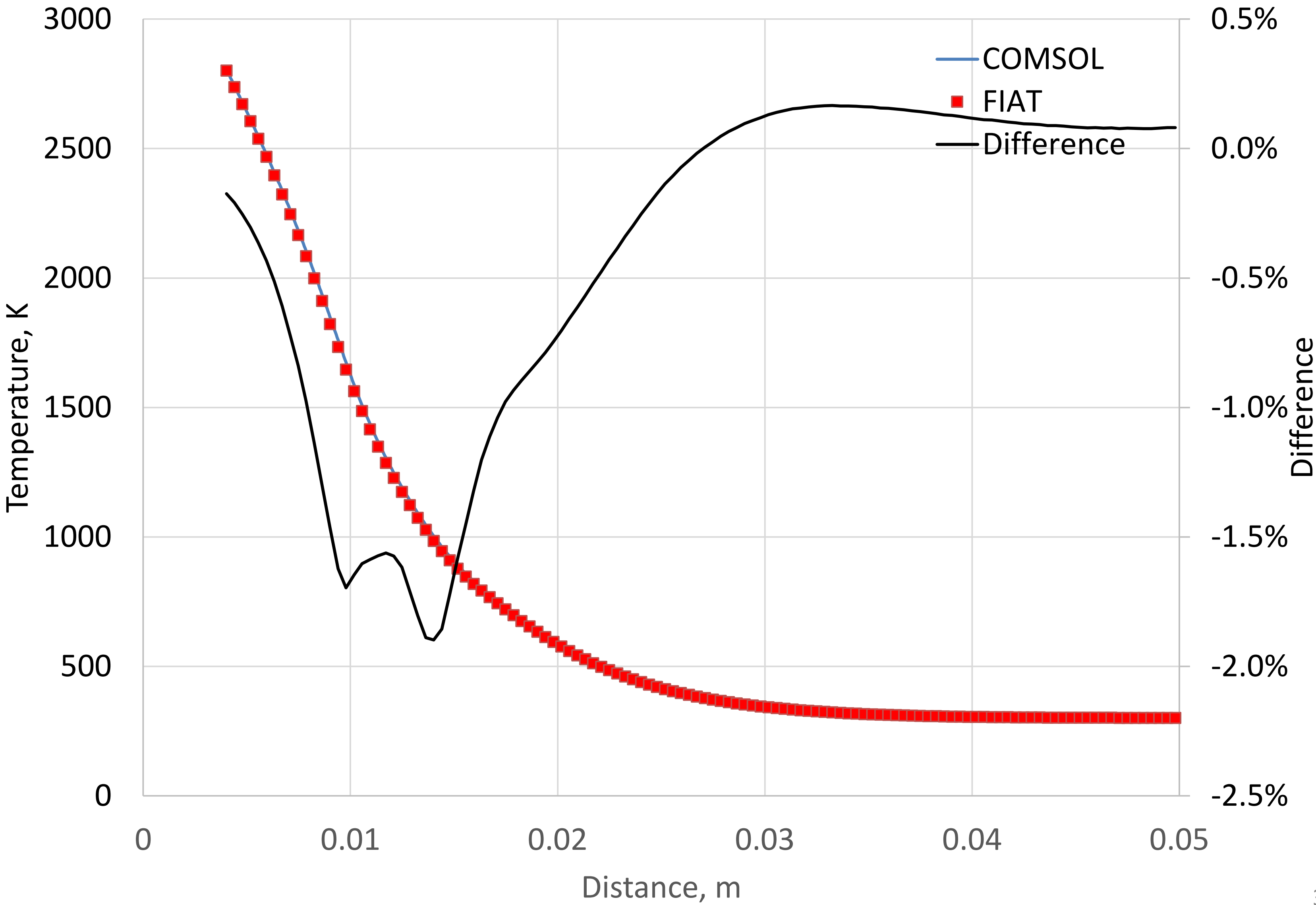
Char and Pyrolysis Surface Mass Loss Rates



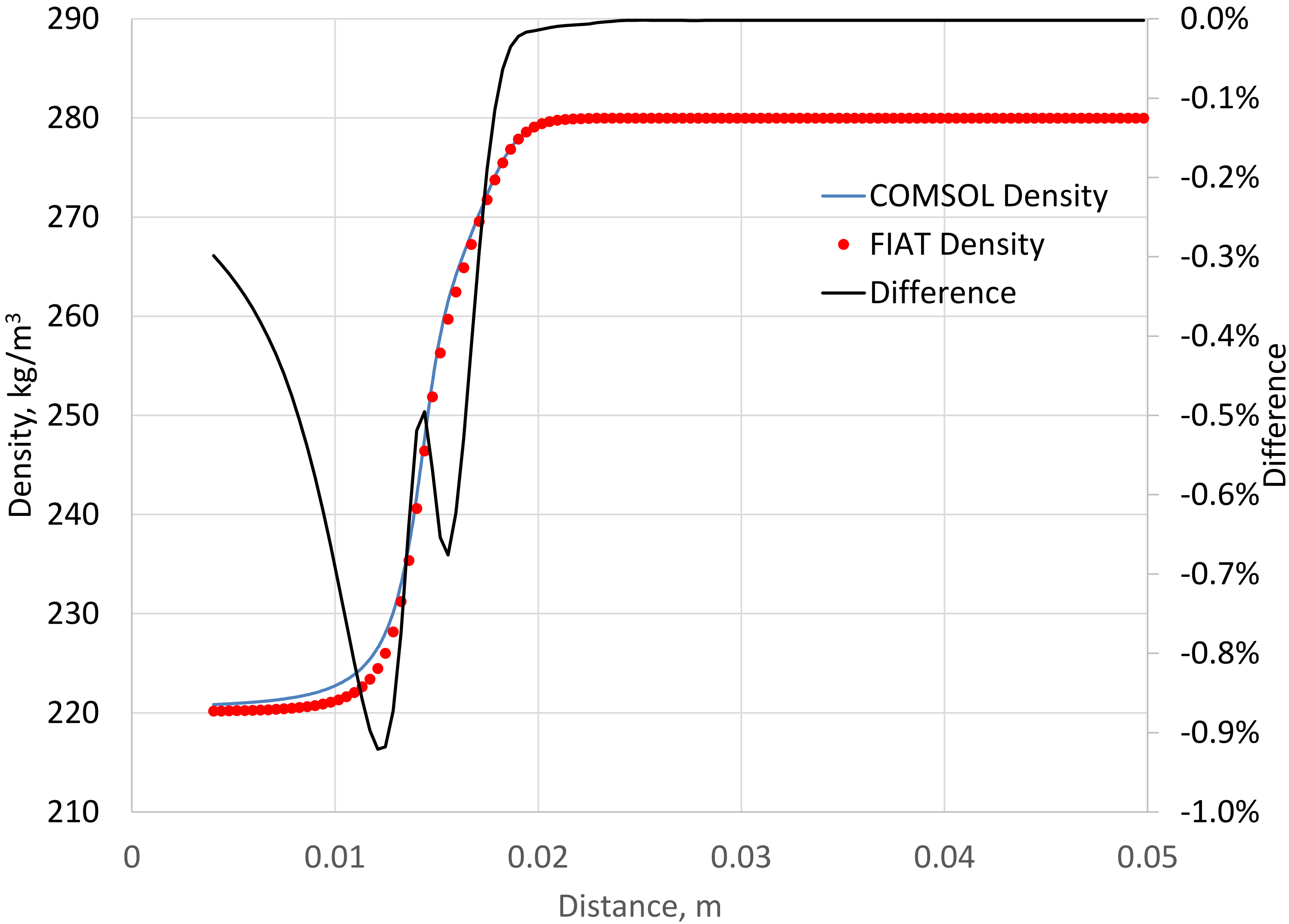
FIAT In-Depth Temperature Comparison



FIAT Temperature Profile Comparison after 60 s



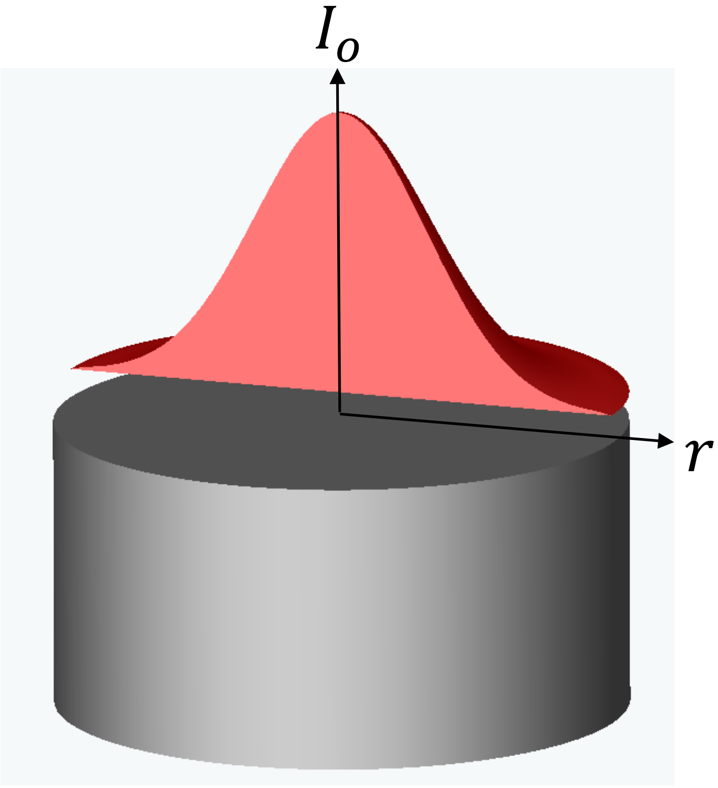
FIAT Density Profile Comparison after 60 s



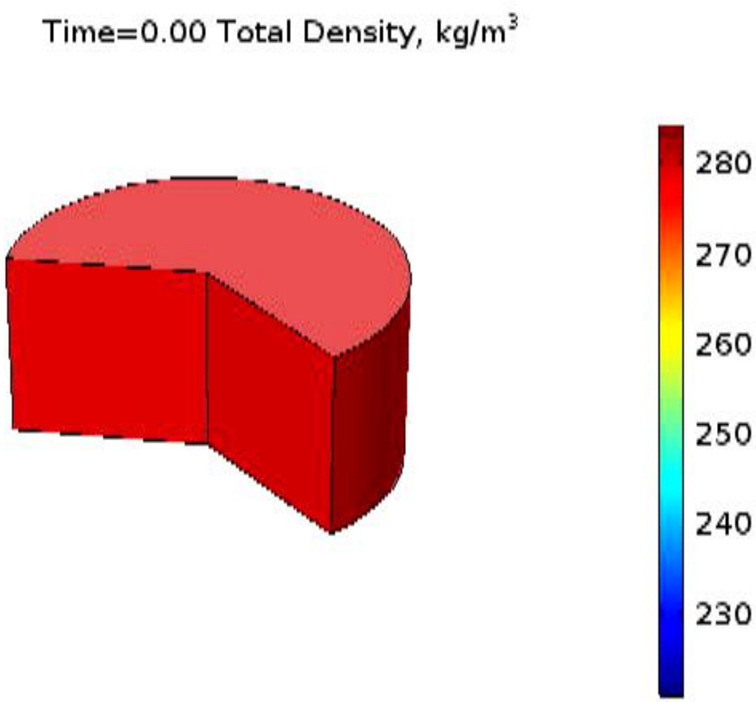
Two-Dimensional Transient Example

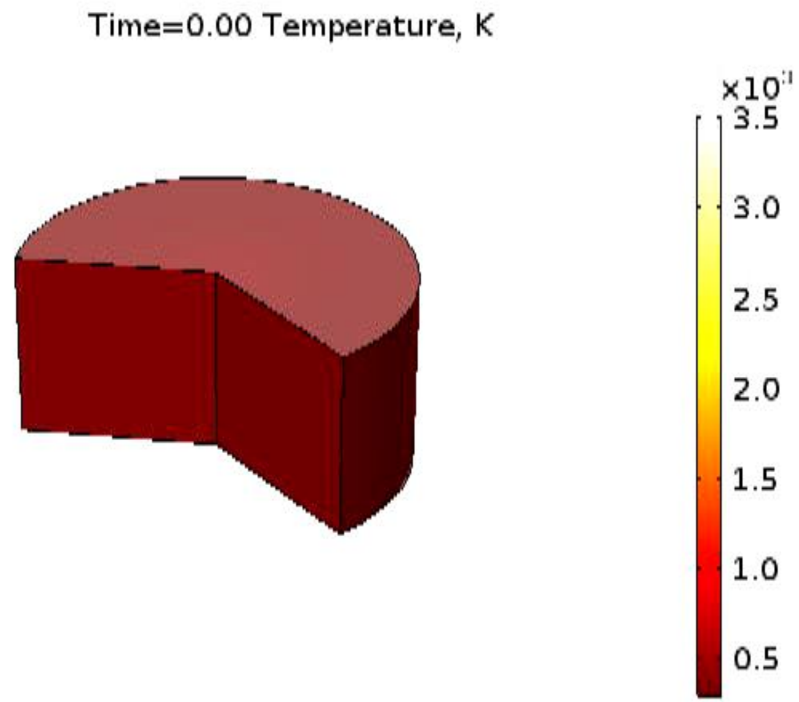
Two-Dimensional Transient Example

- Problem is for a two-dimensional, axisymmetric puck
- Top of puck heated with Gaussian flux profile
- Pyrolysis gas flow calculated from potential flow
- Full surface thermochemistry with recession
- 2-D COMSOL Multiphysics® results compared to a series of 1-D results



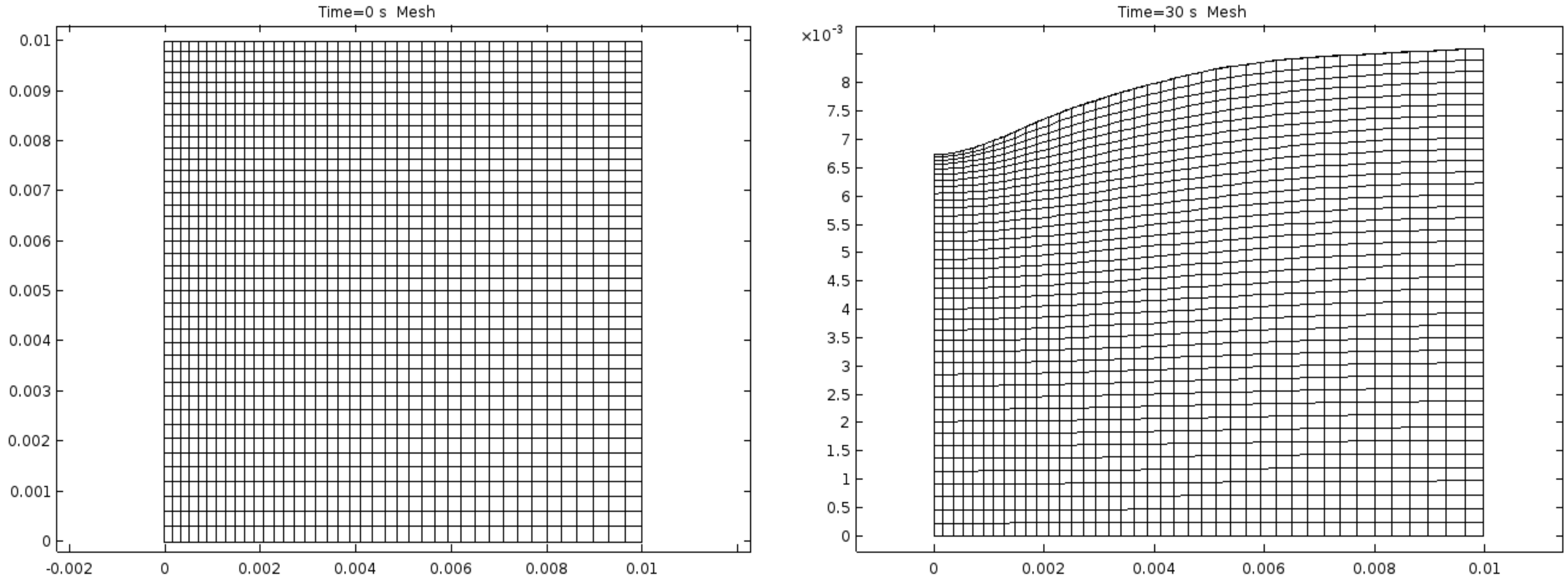
2-D Problem Animation



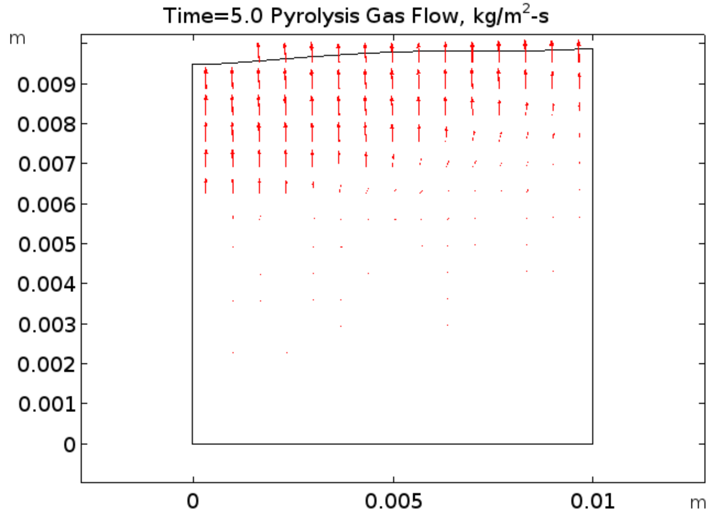


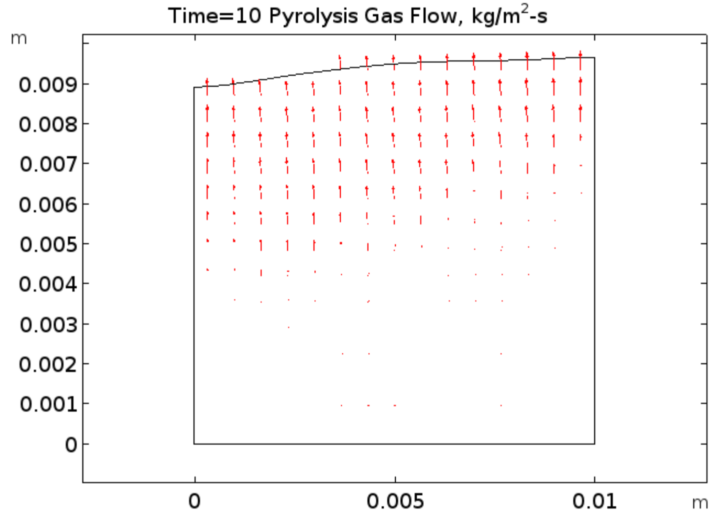
Animation is twice actual speed

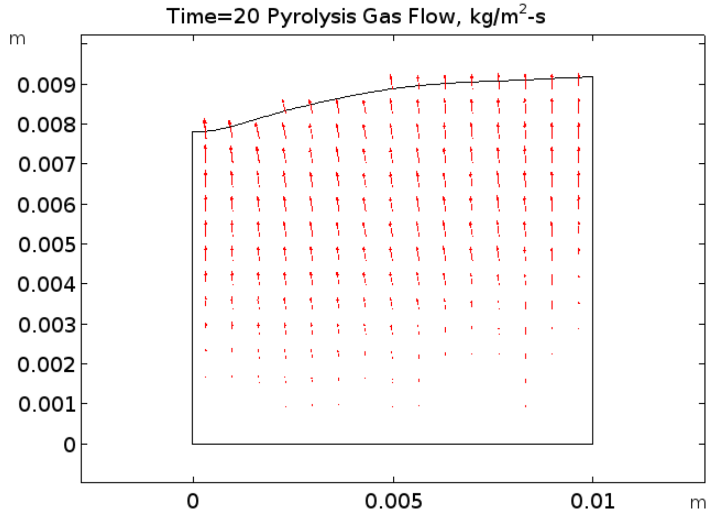
Original and Deformed Mesh

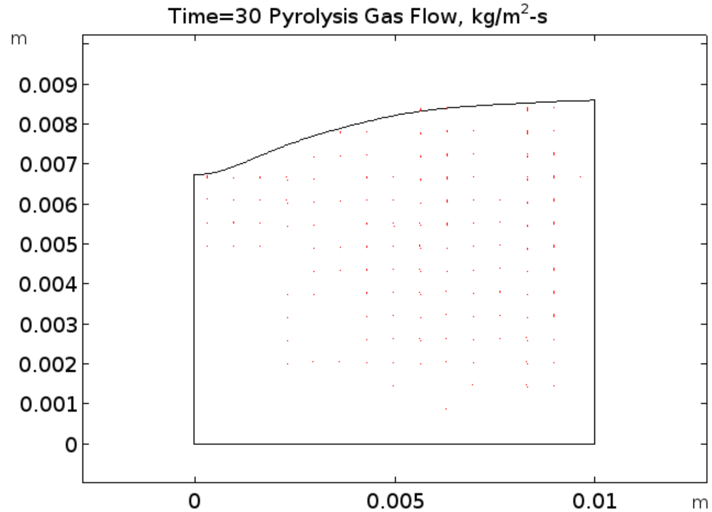


Pyrolysis Gas Flowrate

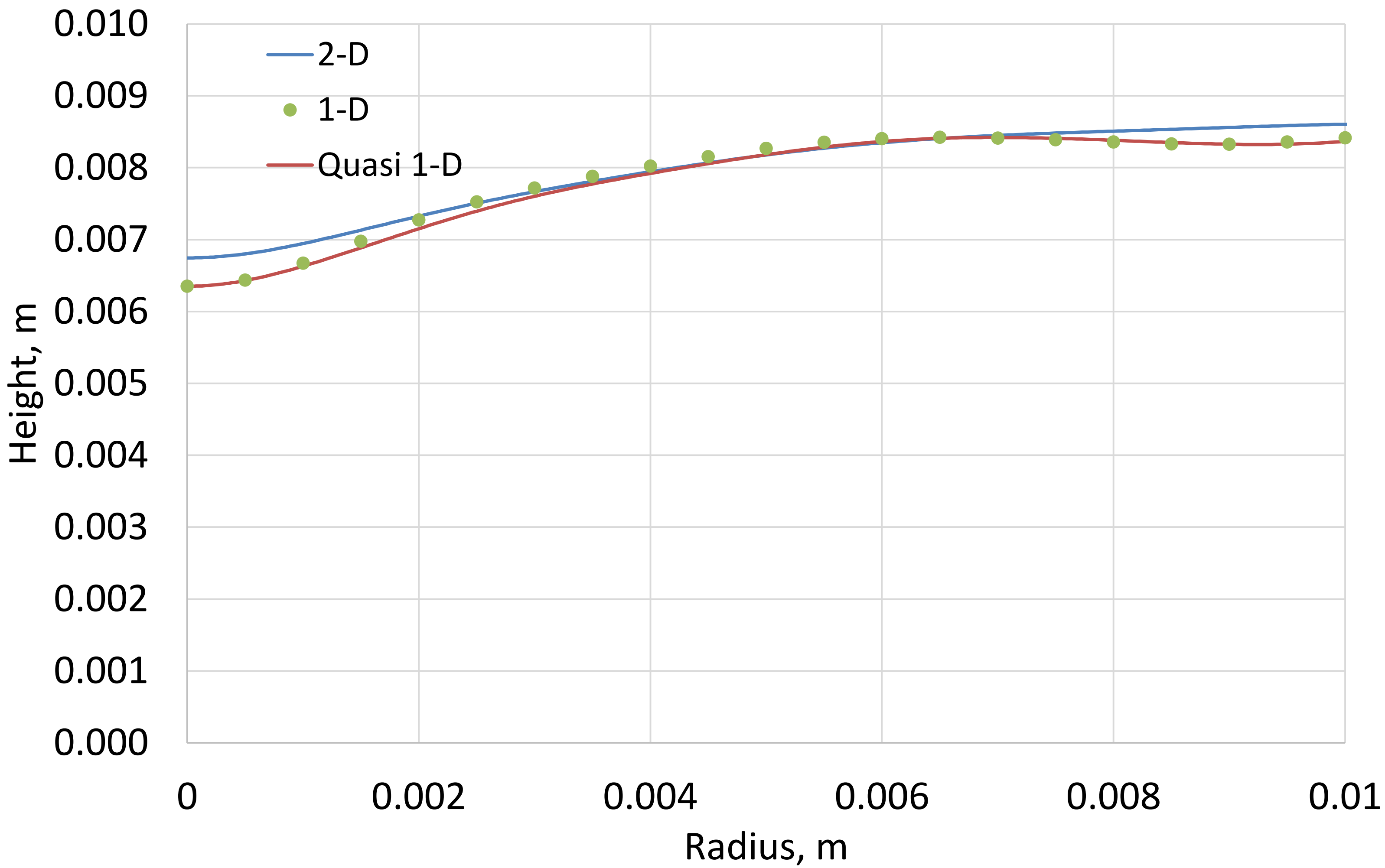








Final Recession Profile at 30 s



Summary

- This work has demonstrated that a commercial finite element code is a suitable tool for modeling pyrolyzing ablative materials
- General capabilities of COMSOL Multiphysics® allow for a wide variety of geometries and problems to modeled
- Code allows for modifications to model to be made quickly and easily
- Advanced solution algorithms are efficient and stable
- Integrated environment provides a very user friendly and powerful system for modeling
- Multiphysical modeling capability allows for structural end external flow to be incorporated into analysis (in progress)